

1.27 ** Since the puck is frictionless, the net force on it is zero, and, as seen from the ground, it travels in a straight line through the center O , as shown in the left picture. It starts from the point A at $t = 0$, travels "due west" with constant speed v_0 , and falls onto the ground at point C after a time $T = 2R/v_0$ (where R is the radius of the turntable).

Now imagine an observer sitting on the turntable near A . As seen from the ground, he is traveling north with speed ωR . Therefore, as seen by the observer, the puck's initial velocity has a sideways (southerly) component ωR , in addition to the westerly component v_0 ; that is, the puck moves initially west *and* south, as shown in the right picture. (The magnitude of the southerly component depends on the table's rate of rotation ω .) As the puck moves in to a smaller radius r , the sideways component ωr gets less, so the puck's path curves to the right. Continuing to curve, it passes through O and eventually reaches the edge of the turntable at point B . The left picture shows the point B of the table at time $t = 0$. The position of B is determined by the following consideration: In the time $T = 2R/v_0$ for the puck to cross the table, point B of the

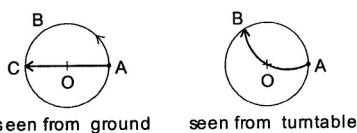


table must move around to point C where we know the puck falls to the ground. Thus the angle BOC is equal to ωT . The faster the table rotates, the larger the angle BOC and the more sharply the puck's path (as seen from the table) is curved.

1.45 ** Since the magnitude of $\mathbf{v}(t)$ is the same as $\sqrt{\mathbf{v}(t) \cdot \mathbf{v}(t)}$, the magnitude is constant if and only if $\mathbf{v}(t) \cdot \dot{\mathbf{v}}(t)$ is. Since

$$\frac{d}{dt}[\mathbf{v}(t) \cdot \mathbf{v}(t)] = 2\mathbf{v}(t) \cdot \dot{\mathbf{v}}(t),$$

this implies that the magnitude of $\mathbf{v}(t)$ is constant if and only if $\mathbf{v}(t) \cdot \dot{\mathbf{v}}(t) = 0$; that is, $\mathbf{v}(t)$ is orthogonal to $\dot{\mathbf{v}}(t)$

1.46 ** (a) As seen in the inertial frame \mathcal{S} the puck moves in a straight line with $\phi = 0$ and $r = R - v_0 t$

(b) As seen in \mathcal{S}' , $r' = r = R - v_0 t$ and $\phi' = \phi - \omega t = -\omega t$. This path is sketched in the answer to Problem 1.27. Initially, the puck moves inward with speed v_0 but also downward with speed ωR . It curves to its right, passing through the center and continuing to curve to the right until it slides off the turntable.

2.2 * According to Stokes's law $f_{\text{lin}} = (3\pi\eta D)v$, which has precisely the form $f_{\text{lin}} = bv$ if we define $b = \beta D$ and $\beta = 3\pi\eta = 3\pi(1.7 \times 10^{-5} \text{ N}\cdot\text{s}/\text{m}^2) = 1.6 \times 10^{-4} \text{ N}\cdot\text{s}/\text{m}^2$.

2.3 * (a) From (2.84) and (2.82), $f_{\text{quad}}/f_{\text{lin}} = (\kappa\rho Av^2)/(3\pi\eta Dv)$. With $\kappa = 1/4$ and $A = \pi D^2/4$, this becomes $\rho Dv/(48\eta)$ or $R/48$, with R given by (2.83).

(b) With the given numbers, $R = 1.1 \times 10^{-2}$ and it is very safe to neglect the quadratic drag.

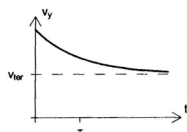
2.4 ** (a) In a short time dt the projectile moves a distance vdt , and the front sweeps out a cylinder of volume $Avdt$. Therefore the mass of fluid encountered is $\rho Avdt$, and the rate at which mass is swept up is ρAv .

(b) If a mass $\rho Avdt$ is accelerated from 0 to v in time dt , the rate of change of its momentum is ρAv^2 . This is, therefore, the forward force on the fluid and, hence, the backward force on the projectile.

(c) Since $A \propto D^2$, it follows that $f_{\text{quad}} = \kappa\rho Av^2 = cv^2$, where $c = \kappa\rho A \propto D^2$. For a sphere in air, $\kappa = 1/4$, $A = \pi D^2/4$, and $\rho = 1.29 \text{ kg}/\text{m}^3$, so $f_{\text{quad}} = (\kappa\rho\pi D^2/4)v^2 = cv^2$, where $c = \gamma D^2$ and

$$\gamma = \kappa\rho\pi/4 = \frac{1}{4} \times (1.29 \text{ kg}/\text{m}^3) \times \pi/4 = 0.25 \text{ N} \cdot \text{s}^2/\text{m}^4.$$

2.5 * With $v_y > v_{\text{ter}}$, the drag force is greater than the weight, and the net force is upward. Thus the projectile slows down, with v_y approaching v_{ter} as $t \rightarrow \infty$. This is clear from Eq.(2.30), as shown in the plot.



2.6 * (a) If we insert the Taylor series for $e^{-t/\tau}$ into (2.33), we get

$$v_y(t) = v_{\text{ter}} [1 - e^{-t/\tau}] = v_{\text{ter}} \left[1 - \left(1 - \frac{t}{\tau} + \frac{t^2}{2\tau^2} - \dots \right) \right].$$

The first two terms on the right cancel, and, if t is sufficiently small, we can neglect terms in t^2 and higher. This leaves us with

$$v_y(t) \approx v_{\text{ter}} t / \tau = gt$$

where to get the second equality I replaced v_{ter} by $g\tau$ as in (2.34).

(b) Putting $v_{y0} = 0$ into (2.35) and then inserting the Taylor series for the exponential, we find:

$$y(t) = v_{\text{ter}} t - v_{\text{ter}} \tau [1 - e^{-t/\tau}] = v_{\text{ter}} t - v_{\text{ter}} \tau \left[1 - \left(1 - \frac{t}{\tau} + \frac{t^2}{2\tau^2} - \dots \right) \right].$$

On the right side, the second and third terms cancel, as do the first and fourth. If we neglect all terms beyond t^2 , this leaves us with $y(t) \approx v_{\text{ter}} t^2 / (2\tau) = \frac{1}{2} g t^2$, since $v_{\text{ter}} = g\tau$.

2.8 * $t = m \int_{v_0}^v \frac{dv'}{-cv'^{3/2}} = \frac{2m}{c} [v'^{-1/2}]_{v_0}^v = \frac{2m}{c} \left(\frac{1}{\sqrt{v}} - \frac{1}{\sqrt{v_0}} \right)$

or, solving for v , $v = v_0 / (1 + ct\sqrt{v_0}/2m)^2$. Clearly, $v = 0$ only when $t \rightarrow \infty$.

2.11 ** (a) Since we are now measuring y upward, the answers can be found from (2.30) and (2.35) by replacing v_{ter} with $-v_{\text{ter}}$:

$$v_y(t) = -v_{\text{ter}} + (v_0 + v_{\text{ter}})e^{-t/\tau} \quad \text{and} \quad y(t) = -v_{\text{ter}} t + (v_0 + v_{\text{ter}})\tau(1 - e^{-t/\tau}).$$

(b) Setting $v_y = 0$ and solving for t , we find $t_{\text{top}} = \tau \ln(1 + v_0/v_{\text{ter}})$. Substituting this time into $y(t)$ we find $y_{\text{max}} = [v_0 - v_{\text{ter}} \ln(1 + v_0/v_{\text{ter}})]\tau$.

(c) In the vacuum $v_{\text{ter}} = \infty$. Letting $v_{\text{ter}} \rightarrow \infty$ in y_{max} and using the suggested approximation for the log term, we find

$$y_{\text{max}} \rightarrow \left\{ v_0 - v_{\text{ter}} \left[\frac{v_0}{v_{\text{ter}}} - \frac{1}{2} \left(\frac{v_0}{v_{\text{ter}}} \right)^2 \right] \right\} \tau = \frac{v_0^2}{2g}$$

since the first two terms in the middle expression cancel each other and $v_{\text{ter}} = g\tau$.

2.16 * As usual, $x = (v_0 \cos \theta)t$ and $y = (v_0 \sin \theta)t - \frac{1}{2}gt^2$. The time to reach the plane of the wall ($x = d$) is $t = d/(v_0 \cos \theta)$ and the ball's height at that time is $y = d \tan \theta - \frac{1}{2}gd^2/(v_0 \cos \theta)^2$. Notice that this height decreases monotonically as v_0 decreases. Thus there is indeed a minimum speed $v_0(\text{min})$ for which the ball clears the wall. Putting $y = h$ and solving for v_0 we find that

$$v_0(\text{min}) = \sqrt{\frac{gd^2}{2(d \tan \theta - h) \cos^2 \theta}}.$$

If $\tan \theta < h/d$, the argument of the square root is negative and there is no real $v_0(\text{min})$; physically, the ball's initial velocity is aimed below the top of the wall, so the ball cannot possibly clear the wall whatever its speed. With the given numbers, $v_0(\text{min}) = 26.4 \text{ m/s}$ or roughly 50 mi/hr.